



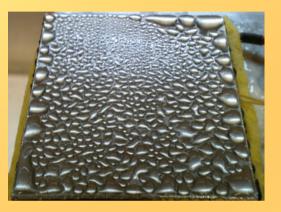


# A Technique of Water Vapor Recovery Through the Characterization of Condensation Phenomena

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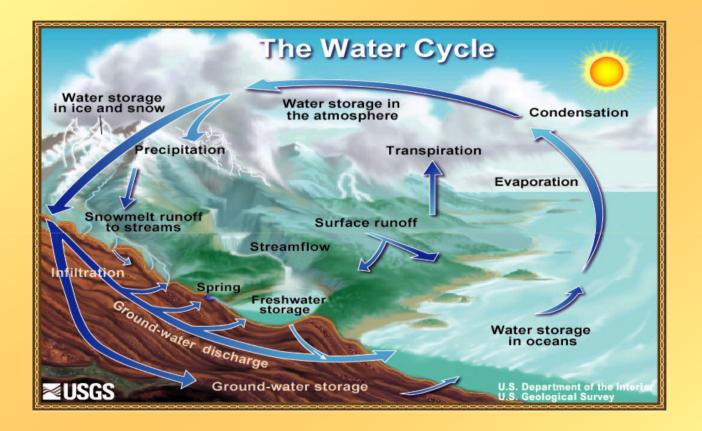
16-18 May 2018 MELiSSA Workshop 2018 CNR. Rome Italy

### *Generation of Potable water by condensation of water vapour from Atmosphere*



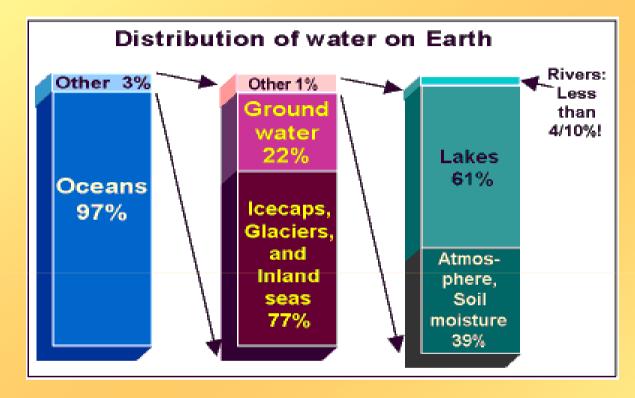
- Our Objectives here, is to study the possibility of using TEC devices to retrieve water condensate from atmospheric air in a closed/open environment.
- And to use this device, where relative humidity is high or temperature variation (Min.-Max.) is high.
- In this study for experimental viavility. we have chosen the specific regions of certain Indian states to study the data and verify the concept, such as Gujarat and Rajasthan, where availability of potable water is a challenge and above parameter is viable.

# Evaporation, Condensation and Precipitation: The main processes of the water cycle



The atmosphere contains more than 12.9 x 10<sup>12</sup> m<sup>3</sup> of renewable water.

# **Distribution of Water on Earth**

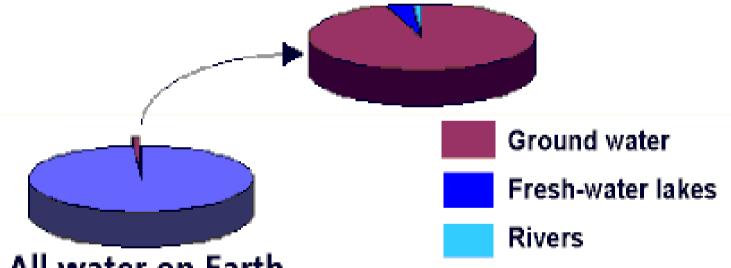


- Most of the Earth's water is in oceans.
- Oceans contain salt water and covers most of the earth's surface.
- Of the final 1%, only 0.4% of water comes from rivers, a major source of the water we use.

# Where is the water we use?

# How much of Earth's water is usable by humans?

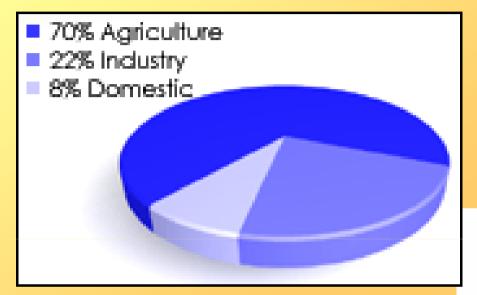
# Water usable by humans

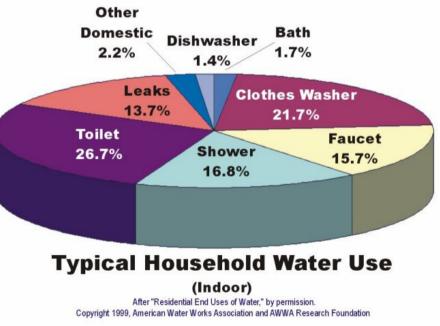


# All water on Earth

0.3% is usable by humans 99.7% is unusable by humans

# Where is Fresh water used for?







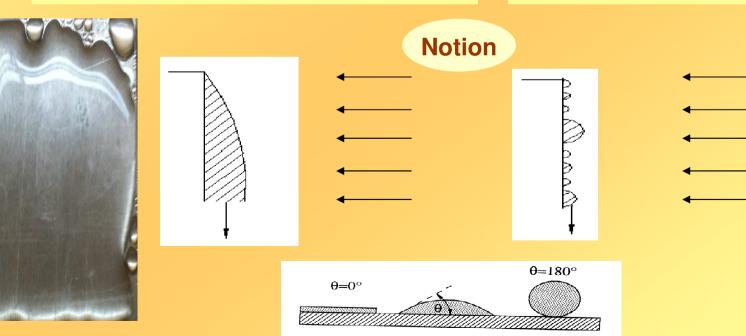
#### **Concept of Study: Basics of condensation**

#### **Condensation**

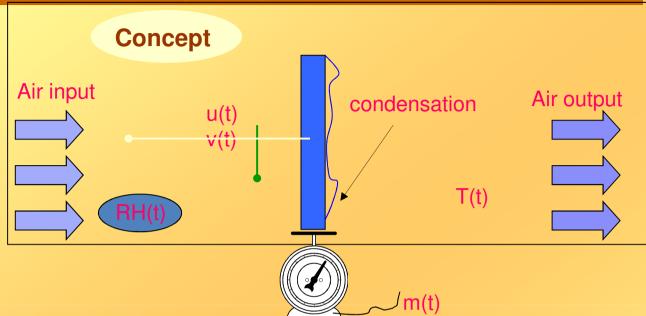
#### Filemwise

# Heat Transfer Coefficient h<sub>film</sub><< h<sub>drop</sub>

- ≻Liquid wets the surface.
- > Continuous film over the surface, that flows down
- the surface under the action of gravity.
- > The layer of liquid condensate acts as a barrier to heat flow, and hence low heat transfer rate.
- >Liquid does not wet the solid surface.
- > Forms separate drops at nucleation sites.
- Drops coalesce to form large drops and
- sweeping clean a portion of the surface, where again new droplets are generated.



#### **Concept of the study: Experimental**



Mean entrance velocity (0.0 - 5.0 m/s), Temperature (18-35) °C, Controlled RH 25-90 %

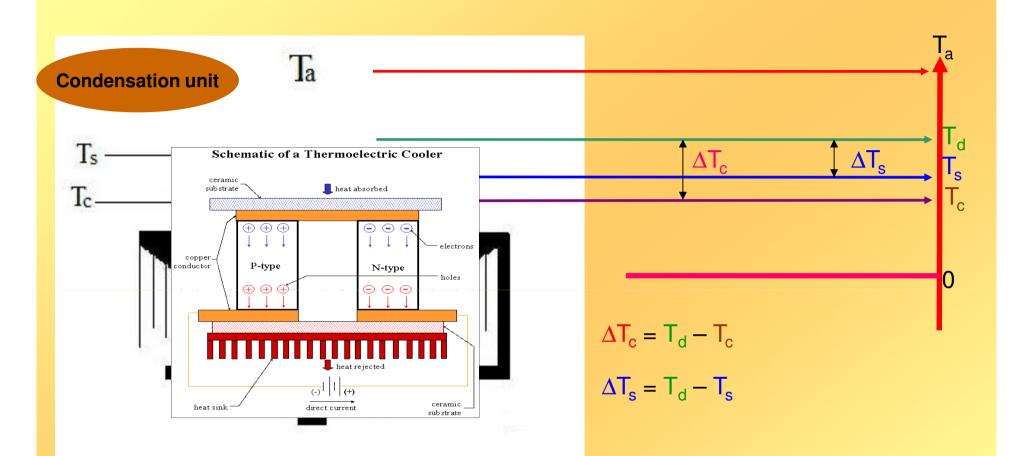
#### Dry phase

- Validation of concept : Characterization of wind flow and temperature profile
- Choice of simple geometries & surface material

#### Humid phase

- Condensation of water vapour from humid air in an open environment (In a Room)
- Validation in a controlled conditions (Inside the wind tunnel)
- Modeling of results

#### **Condensation unit and Temperature profiles**

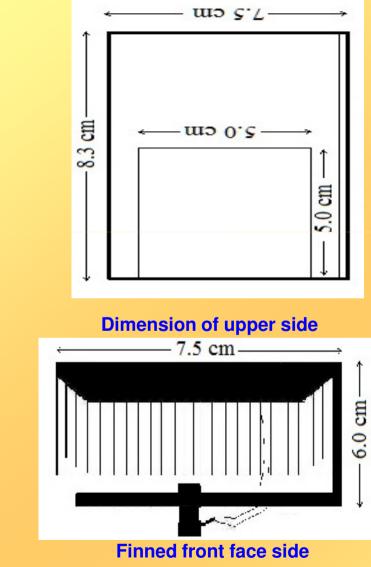


Basic questions one has to deal with :-

- 1. Choice of Material, its thickness, size and proper heat sink for removal of heat from hot side
- 2. Measurement of different temperatures
- 3. Characterization of flow profile on its active surface



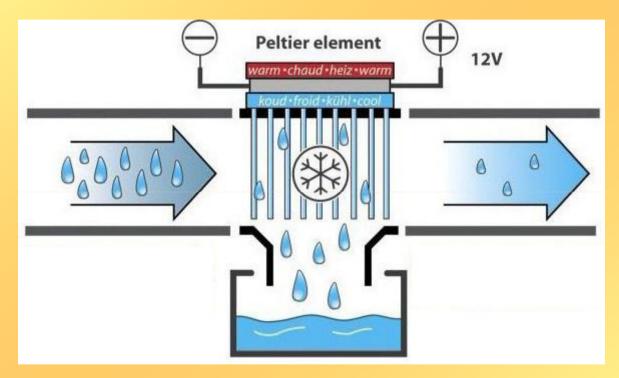
## **Device Dimensions of condensing unit**





# **Use of Peltier Device**

#### **Tentative Schematics:**



# Challenges in this study:

- Development of a low cost technique to produce the drinking water from humid air.
- To create a low temperature surface which may produce water condensate.
- To enable tuning of the cold surface for regulating temperature.
- To create a technological viable solution at low price for drinking water production.
- To locate the regions, where this kind of device may be fruitful.

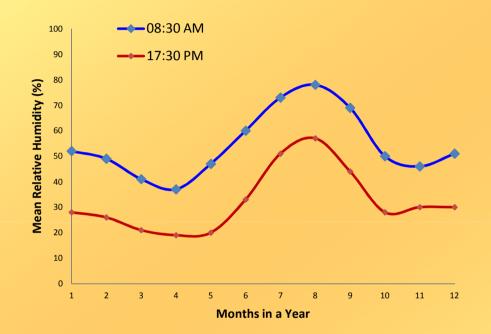
### **Estimation of water condensation**

To calculate the amount of water that one can condense on a TEC device cooled at  $10^{\circ}$ C. The following equation for the generation of water from ambient air may be used\*:

$$L_{w} = \frac{(H_{x}^{\phi} - H_{10}^{100\phi})}{100} \times E$$

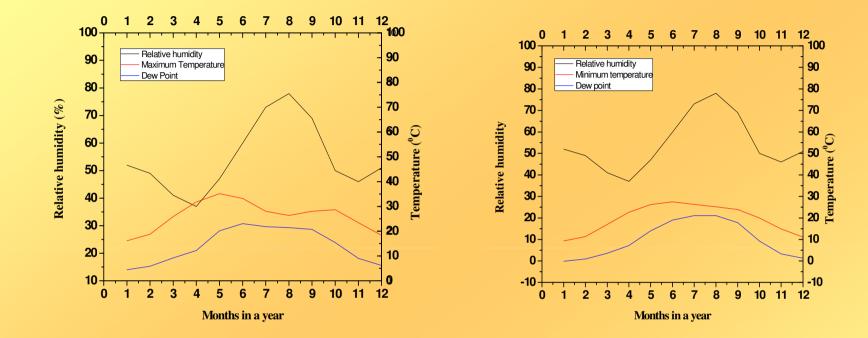
Where  $L_w$  is the generated liquid water (g/m<sup>3</sup>), H<sub>x</sub> absolute humidity at any point (g/m<sup>3</sup>), H<sub>10</sub> absolute saturated humidity at 10 °C (g/m<sup>3</sup>), E the efficiency of the TEC device (it's the ratio of the amount of the water extracted to the total moisture content of the air).

#### Yearly Temperature distribution at some Districts of Rajasthan



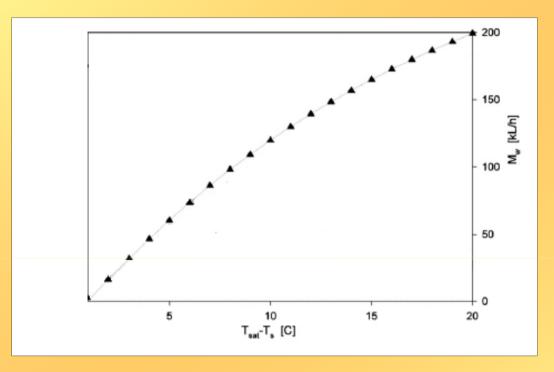
PLOT SHOWS MONTHS IN A YEAR VERSUS THE MEAN RELATIVE HUMIDITY IN TWO TIMES AT A DAY TIME IN UTC AT 3 (i.e. 08:30 IST) AND 12 (i.e. 17:30 IST)

#### Yearly Temperature distribution at some Districts of Rajasthan



PLOT SHOWS THE MONTHS IN A YEAR VERSUS THE VALUES OF MEAN RELATIVE HUMIDITY, MAXIMUM AMBIENT AND DEW POINT TEMPERATURE. PLOT SHOWS THE MONTHS IN A YEAR VERSUS THE VALUES OF MEAN RELATIVE HUMIDITY, MINIMUM AMBIENT TEMPERATURE AND DEW POINT TEMPERATURE.

#### Trend of water production as a function of temperature difference

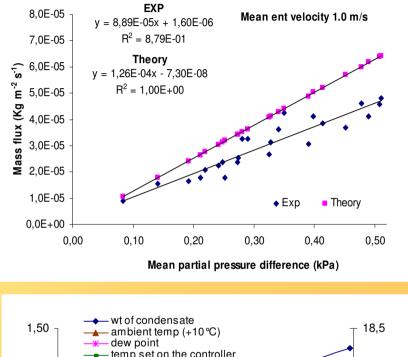


AMOUNT OF FRESHWATER PRODUCED AS A FUNCTION OF THE TEMPERATURE DIFFERENCE BETWEEN THE DEW POINT AND THE SURFACE TEMPERATURE AT AMBIENT TEMPERATURE T = 50 °C [1].

### **Theoretical Estimation: Water Production**

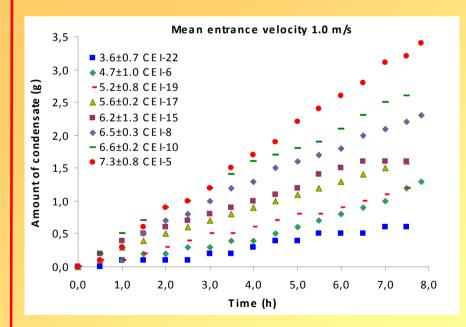
- The amount of water can be condensed with a TEC device capable to condense 50% of the water present in air (50% of efficiency), with an air flow of 1 m<sup>3</sup>/s.
- Example:- A normal day in August in Uttar Pradesh (India), the temperature is 35 °C and the RH 80%. So the amount of water that is theoretically possible to condensate is 1927 L per day, 700kL/yr.
- On an average, An Indian household uses 135 L/day of water, 50kL/yr [\*]. Thus, this system may be sufficient for 14 Indians.
- So, the water production is significant, but too low to meet the needs of a city where it would be necessary to multiply these systems.
- > For example it would take more than 12,00,000 devices to supply New Delhi.
- In the best case (unlikely circumstances) the price is 68.2\$ for 1 m<sup>3</sup>. The largest price in France for 1 m<sup>3</sup> is 5.50 €, 7.15 \$. It costs almost ten times the price of potable water in France. [\*]

#### **Inside closed system: Condensation mass flux**



- temp set on the controller (i) 1,20 4 (i) 0,90 (i) 0,60 (i) 0,30 15.5 Temperature (°C) 12,5 9,5 6.5 3.5 0,00 2,0 5,0 0,0 1,0 3,0 4,0 Time (h)

Amount of condensate versus time with different average temperature difference ( $\Delta T_c$ ) for 1.0 m.s<sup>-1</sup>



#### Mass flux calculations: In a closed system

For a flat plate in a parallel flow (laminar)

$$\overline{Sh_L} = 0.664 \operatorname{Re}_L^{1/2} Sc^{1/3} \qquad 0.6 \le Sc \le 50$$

For turbulent flow, the local Sherwood number

 $Sh_L = 0.0296 \operatorname{Re}_L^{4/5} Sc^{1/3}$   $0.6 \le Sc \le 300$ 

Re = 
$$\rho_{\infty}UL/\mu_{\infty}$$
  
Sc =  $\mu_{\infty}/\rho_{s}D$   
Sh = kL/D

Where

And if it is a mixed type of flow, with a mixed boundary layer laminar/ turbulent, the leading edge has a laminar boundary and approaching the rear edge it is turbulent, then

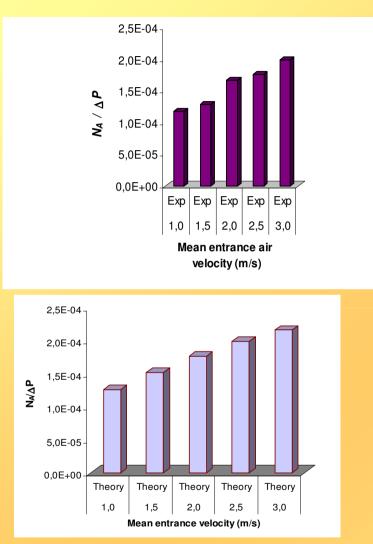
2 
$$Sh_L = 0.037 \operatorname{Re}_L^{4/5} Sc^{1/3}$$

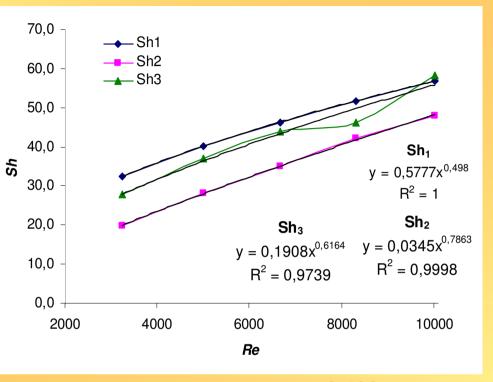
Mass flux (Asano, 2006)

$$N = \frac{Sh\rho_s D(\omega_{\infty} - \omega_s)}{L}$$

- Re = Reynolds Number Sc = Schmidt Number Sh = Sherwood Number
- U = Mean air velocity at Free stream (m/s)
- *L*= characteristic length (m)
- $\rho$  = density (kg /m<sup>3</sup>)
- $\mu$  = dynamic viscosity (Pa.s)
- $\omega$  = mass fraction of water vapour in air
- $D = Diffusion Coeff (m^2/s)$

#### **Conclusions For a closed system**





 $Sh_1 = X_1. Re^{0.498}$  $Sh_3 = X_3. Re^{0.616}$  $Sh_2 = X_2. Re^{0.786}$ 

# The relation modeled for a flat plate configuration:

 $Sh = 0.225 \,\mathrm{Re}^{2/3} \,Sc^{1/3}$ 

Where 3000 < *Re* < 10000 *Sc* = 0.6

#### Table of water parameters compare with standard values

Parameters	Unit	Requirement (A corptable Limit)	Desirable limit	Maximum Permissible limit	Result of Sample	Distilled water	Test Protocol
			(IS 10500-2012) Second Revision				
Colour	Haten	15 true colour unit [1]	5.0	15	< 50	ND(8)	2120 B, APHA 23 2017
Turbidity	NTU	5 Nephelometric Turbidity unit (NTU) [1]	10	5.0	0.0	0.07 [8]	2310 B, APHA 23 <sup>41</sup> 2017
Chiloride (C2.)	mg/L.	5 mg/L [1]	2.50	1000	8.0	ND(S)	4500-C1 B, AP11A23*2017
Electrical conductivity	µз/ст	0.005-0.05 S/m*[2]			58,02	28 (µa*cm)[5]	2510 B, APHA 23" 2017
Total Hardness (as CaCo <sub>3</sub> )	mg/L.	500mg/L as cald un carbonale [1]	200	600	0.0	0.3 mg/l. [71	2540 C, APHA 23 <sup>th</sup> 2017
Iron (Pc)	mg/L.	0.4 mg/L [1]	.3	No Relatation	"HDL	Less than 1 (mg/kg)[4]	3500Pe-B, APEA 23 <sup>ed</sup> 2017
Magnerdum (Mg)	mg/L.	10.5 mg/L[1]	30	No Relatation	0.0	Less than 1 (mg/kg)[4]	3500-8, APEA 25" 2017
pH		6-8 [1]	6.5	8.5	7.5	65-7.5	4500-H*H APHA 23" 2017
Sulphate(Sol4)	mg/L.	500 mg/L [1]	200	400	8,12	Less than 2 (mg/kg)[4]	4500-50 4 APEA23*2017
Total Dissolved Solids	mg/L.	1000 g/L [1]	500	2000	101	11 mg/L[4]	2540D, APHA 23 <sup>rd</sup> 2017
Alkalinily ( as CaCo <sub>2</sub> )	mg/L.	200 mg/L [3]	200	600	20.0	0.52[8]	2320B, APHA 23" 2017
Nitrale(NO <sub>3</sub> )	mg/L.	50 mg/L [1]	45	No Relatation	1.12	.930 (mg/L) [2][4]	4500No5 B,A199A25 <sup>42</sup> 2017
Phoetide (12)	mg/L.	1.5 mg/L [3]	1.0	1.5	0.22	0.002 [8]	4500F/B, APHA 23 <sup>th</sup> 2017
Calcium (Ca)	mg/l.	75 mg/L [3]	7.5	200	0.0	Lens than 5 (mg/kg)[4]	3500B, APHA 25" 2017

\*BDL - Below Detection Limit

#### Real research

1. Cataloburyler detailing main goally standards in developing cousts in (Report) W1007 and a Science, Wiger. America Line, 2001.

2. Water completely solution - Leasting higher ways brackeds and index him-

Degl Index Standard, Debiling units - specification, Record Revision of 2110200, Research Index - Namberla (1920), 823 No. 13,055 20

6. Real Applican Directory, Distilled water - Specification, DAX 123 (1999)

- Characterized properties of tag and detilled and excharged process maintaining and articles, image 421(8), 9822. 4.161.0822 [doi:10.1016/j.0822.0010
- Main Assessment, Chaine strip Of Referantian Line site, http://hep-press.out.edu/assessment/hep-01091073379

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